



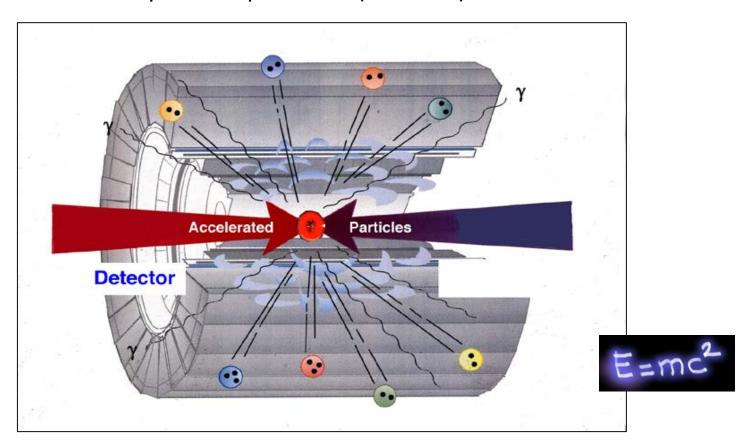
### 1. Concept: $E = mc^2$



How to discover new (elementary) particles?

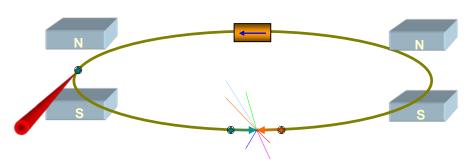
✓  $E = mc^2$ , produce particles from a spot of energy and seek...

We need E, an energy production unit (accelerator-collider), and an experiment to look at the shower of particles produced (detector).





# Concept: Colliders, circular vs. linear



Collision energy

$$E_{TeV} \cong 0.3 B_T R_{km}$$

9 T & 4.6 km → 14 TeV

#### **Circular Collider:**

- Many magnets & few cavities, need higher magnetic field for a smaller ring
- High energy but growing synchrotron radiation losses ( $\propto E^4/R$ )
- High luminosity by a high bunch repetition rate
- Main bill is for the cryogenics for running the compressors to get 4 K.



#### **Linear Collider:**

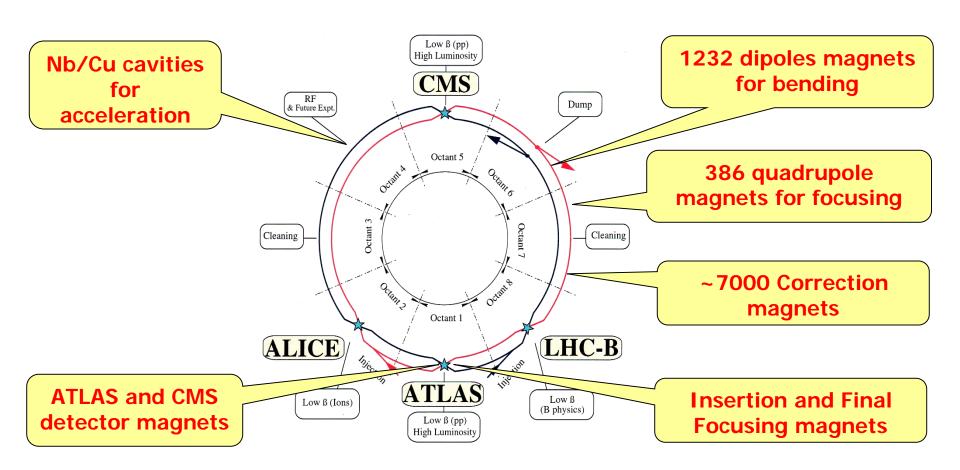
- Few magnets but nearly all cavities, need efficient RF power production
- A higher gradient will give a shorter machine
- Single shot, requiring a very small cross-section for high luminosity
- Main bill Is for the RF power.

# Example: Large Hadron circular Collider Exploring the energy frontier between up to 13-14 TeV using proton-proton & Pb-Pb collisions CMS ALICE LHC ring,27 km circumference



### HE Physics and Superconductivity

LHC (and many other accelerators) can not be realized without extensive use of Superconductivity and High Quality Magnets



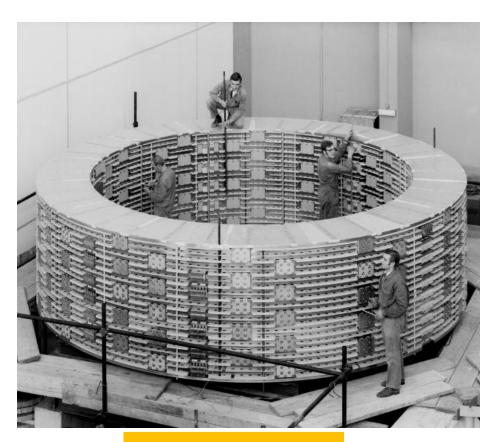
No Higgs without Superconductivity!



# Large HEP detector magnets of the past...



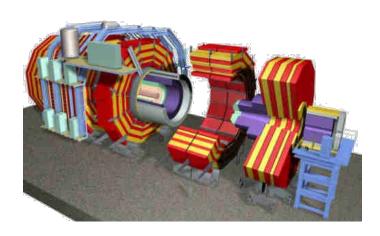
Omega, medio 1972



BEBC, medio 1973

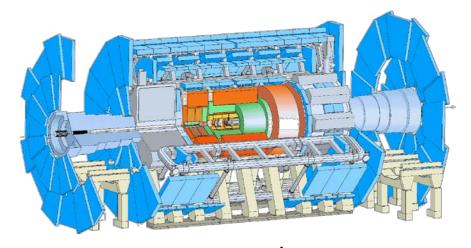


### ... and present detectors, CMS and ATLAS

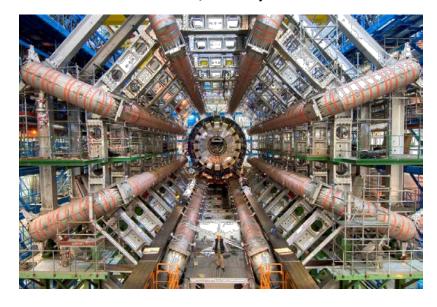


CMS (2008)





ATLAS (2008)



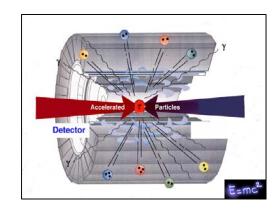


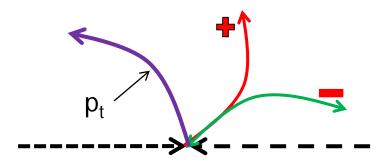
# Concept: why magnetic field in detectors

How to analyze the shower of particles? We need:

- Track reconstruction
- Energy measurement (in calorimeters)
- Charge identification in magnetic field
- Momentum measurement in magnetic field.

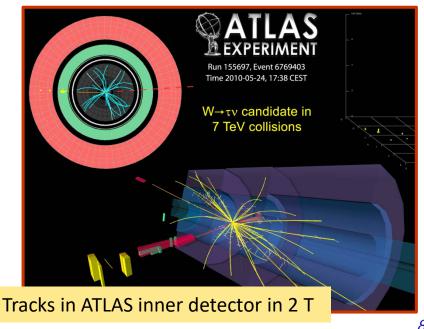
A detector magnet is in fact a "magnetic separator".





### Information yield:

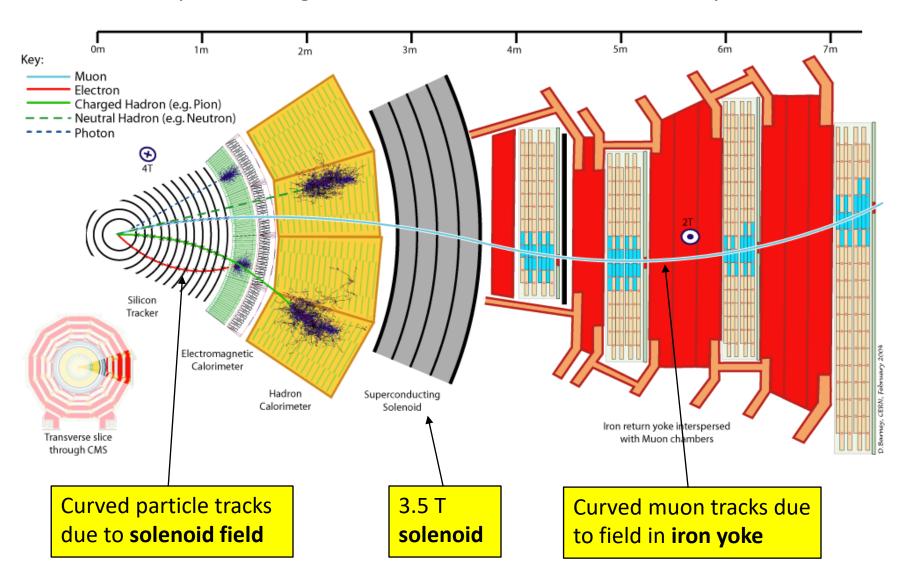
- left turn => positively charged particle
- right turn => negative particle
- curvature => momentum





# Concept: charged particle tracking

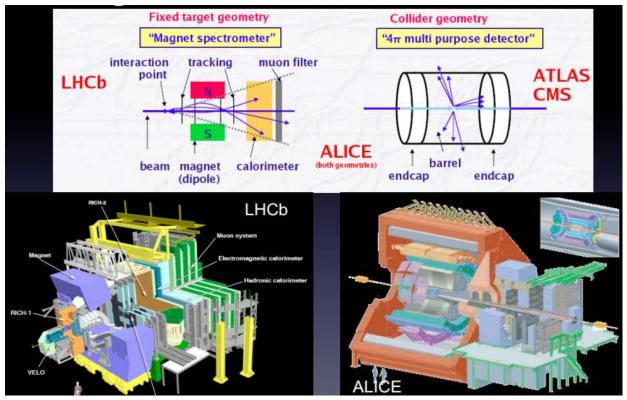
Example: tracking in the CMS Solenoid and iron return yoke

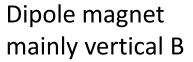




### Concept: type of magnet used

- There are 3 principle magnet layouts for particle bending
- Choice depends on type of experiment and " $4\pi$ " or single direction fixed target, or even a combination of these, all variants exist.







Solenoid + yoke mainly axial B



Toroid + Solenoid

Toroid + Solenoid
Tangential + axial B



### Concept: sizing the detector

What determines the size of a generic " $4\pi$ " detector and its magnetic field?

#### Radial thickness

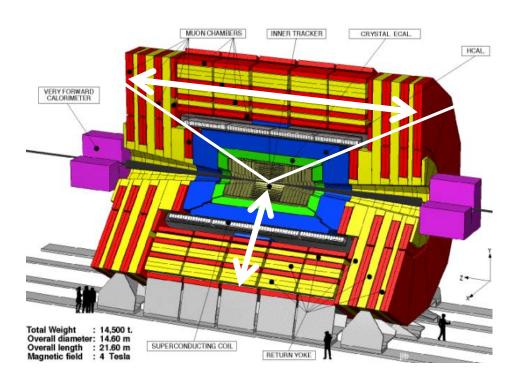
#### is the summation of:

- + tracking length inner detector
- + thickness of the solenoid
- + radial build of the calorimeters
- + tracking length
- + thickness of shielding iron yoke

### **Axial length**

#### is the summation of:

- + "catch angle" in forward directions sizing the length of the solenoid
- + thickness of iron shielding.





### Concept: sizing the detector

#### What counts is momentum resolution!

A particle with charge q and momentum p<sub>t</sub> traveling through B is bent by Lorentz force

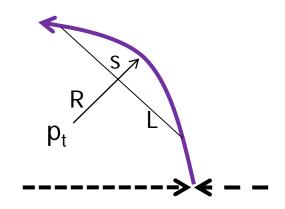
$$F = q (E + v \times B) \qquad (E \cong 0)$$



$$s = L/_{8R} = \frac{qBL^2}{8p_t}$$

and momentum resolution

$$\frac{\partial p_t}{p_t} = \frac{p_t}{0.3BL^2}$$



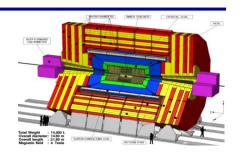
p <sub>t</sub> (GeV/c)	s [mm] @ B=1T, L=1m
1000	0.037
100	0.37
10	3.7
1	37

- Keeping at minimum the resolution for higher collision energies, so higher momenta, requires to scale up the detector up with BL<sup>2</sup>!
- 10 times more energy  $\rightarrow$  2xB and  $\sqrt{5}$ =2.4x tracking length, say diameter,
- and the axial length grows accordingly!
- Thus: detectors scale in size with the collision energy!

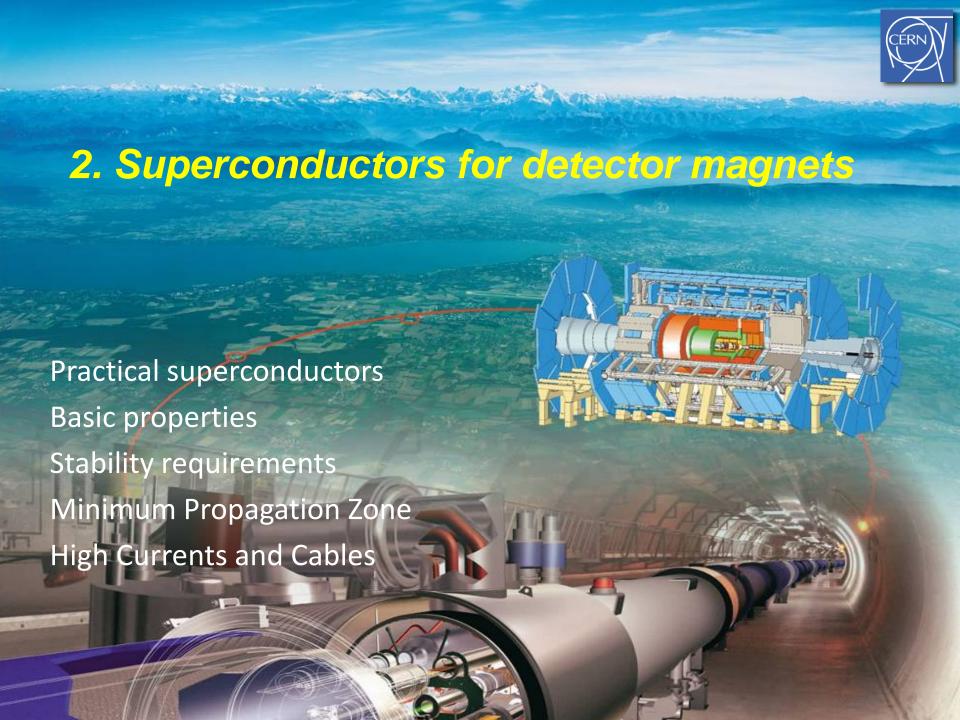


### **Concept:** more requirements

- (1) Momentum resolution → sufficient BL<sup>2</sup>
- (2) For physics we need B, not the magnet (!), though a rewarding challenge for magnet engineers!

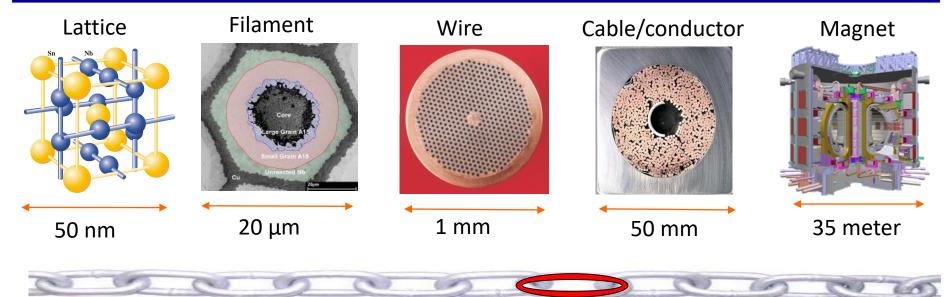


- → Minimum thickness of coils to minimize particle scattering (especially when the calorimeters are put outside the central solenoid!)
- → Material?: in general all Al, low density, when inside the calorimeters
- (3) Hermetically closed detector catching all particles
  - → Minimum lost sphere for magnet services and supporting structures.
- (4) Full integration of magnets with detectors interleaved and supported
- (5) Always working to avoid loss of data
  - → Requiring high operational margins in terms of temperature and current
- (6) Unique and not replaceable (can not really be repaired)
  - → Very robust design with large margins and high level of redundancy
- (7) And yes, low cost as well!
  - → Use NbTi superconductor at 4.5 K





### From materials to magnets

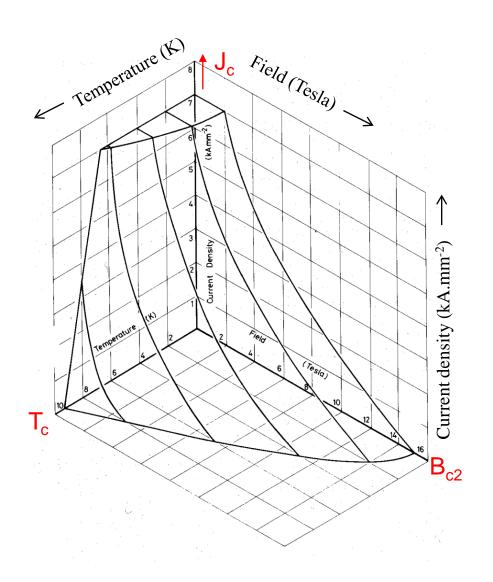


How to make performing multi-kA conductors that guarantee the magnet not to quench or degrade ?

- → We need to understand and control the entire chain
- An under developed area of research, but essential to avoid surprises and degraded magnet performance
- Striking examples exist of missing understanding putting large projects at risk



### Practical Conductors, NbTi



Cubic alloy, isotropic





Tc: 11 K Bc<sub>2</sub>: 13 T

Very well developed ~1 €/ kA m



### Critical properties of type II superconductors

### **Critical Temperature T<sub>c</sub>:**

$$3.5 k_B T_c = 2 \Delta(0)$$

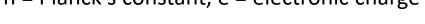
 $k_B$  is Boltzmann's constant, D(0) is the *energy gap* (binding energy of Cooper pairs) at T= 0.

### **Upper critical field Bc<sub>2</sub>:**

Flux is penetrating a type II superconductor through flux lines, a "tube" in the material in normal state enclosing the flux quantum

$$\phi_o = \frac{h}{2e} = 2 \times 10^{-15} Weber$$

h = Planck's constant, e = electronic charge



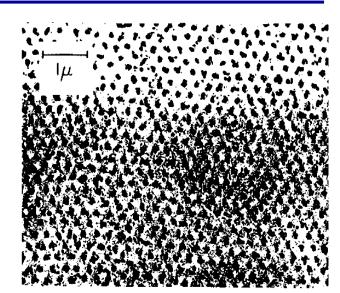


$$B_{c2} = 3.1 \times 10^3 \ \gamma \ \rho_n \ T_c$$

where  $r_n$  is the normal state resistivity

! Best superconductors are best resistors!

T<sub>c</sub> and B<sub>c</sub>, are intrinsic material properties





### **Critical current density**

Flux lines consist of resistive cores with supercurrents circulating round them.

The spacing between flux lines:

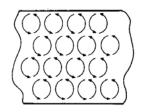
$$d = \left\{ \frac{2}{\sqrt{3}} \frac{\phi_o}{B} \right\}^{\frac{1}{2}} = 22nm \quad at 5T$$

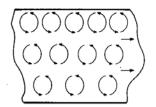
A uniform distribution of flux lines gives no net current, so  $J_c = 0$ ,

but a gradient produces a net current density:

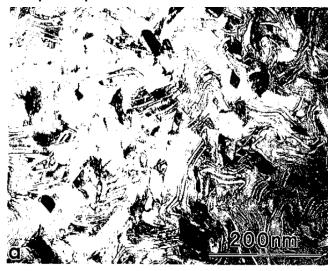
$$\nabla x B = \mu_o \ J = J_c$$

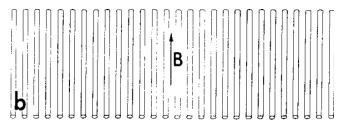
- gradients are introduced by inhomogeneities in the material, like dislocations, precipitates
- process is known as flux pinning
- flux pinning is an irreversible process leading to AC losses





precipitates of  $\alpha$  Ti in NbTi

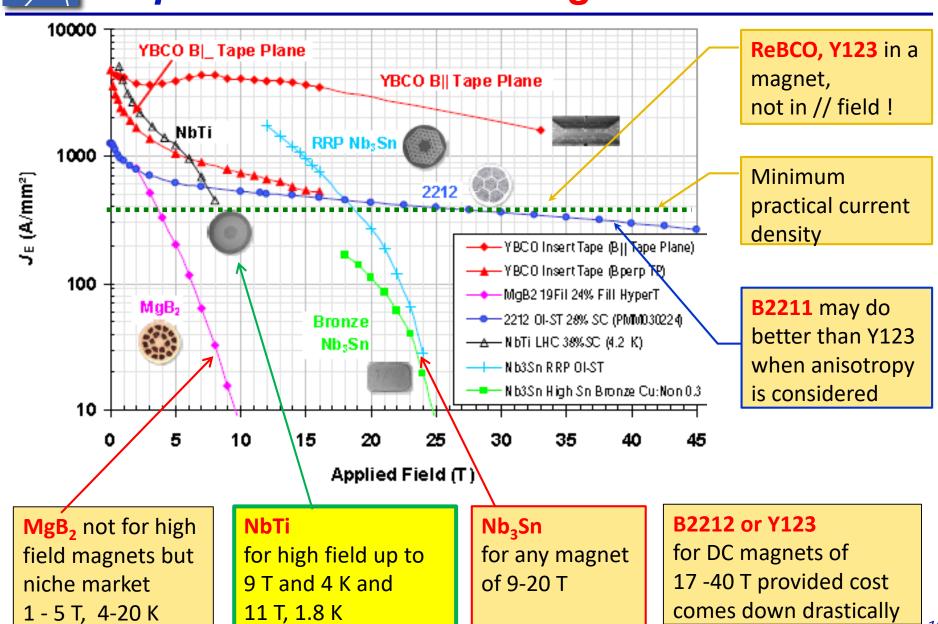




Flux lines lattice at 5 T, same scale.



### Superconductors for magnets





### Example: Superconductors in ATLAS Detector

#### Barrel Toroid Conductor: 65 kA at 5 T

- 1.25 mm diameter NbTi/Cu strand, 2900 A/mm<sup>2</sup> at 5 T
- 40 strands Rutherford cable, ~1700 A / strand
- Co-extruded with high purity Al (RRR>1500)
- Intermetallic bonding Cu-Al is required
- size 57 x 12 mm²,
- 56 km made
- Production by 2 suppliers

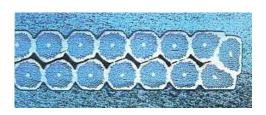
For the End Cap Toroids, size 41 x 12 mm<sup>2</sup>,

26 km made

For the Central Solenoid, size 30 x 4.3 mm<sup>2</sup>

9 km made (Ni/Zn doped Al for higher Y-stress)









### Coils and Superconducting Windings

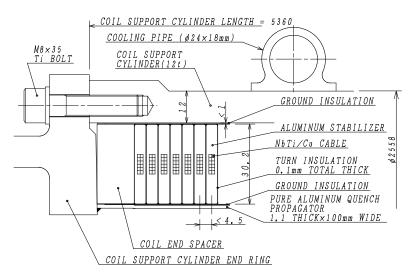
### As argued before, we need:

- 1 5 T, so we use NbTi
- thin and transparent, so we use Al
- simple cooling and robust mechanics.

This caused an evolution of detector magnet design since some 40 yrs.

#### We see:

- Al stabilized Rutherford cables made from NbTi/Cu strands.
- 1-4 layer coils, often wound inside a supporting cylinder taking the hoop stress.
- Conduction cooled by thermo-siphon or forced He flow cooling at 4.5 K through Al tubes on the support cylinder.



Typical coil windings (ATLAS solenoid)



ATLAS Solenoid 2.5 T

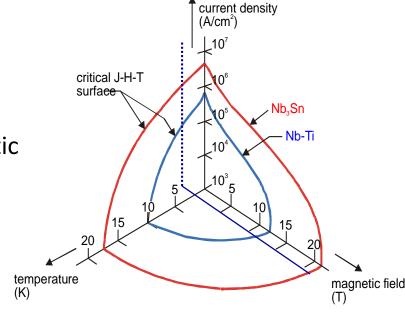


### Critical temperature, field dependency

Superconducting Phase (J<sub>c</sub> vs. B and T).

For maintaining the superconducting state, the conductor must operate below the critical surface determined by critical current, magnetic field and temperature.

For NbTi the critical area is bounded by:



$$T_c(B=0) = 9.2 \text{ K} \text{ and } B_{c2}(T=0) = 14.5 \text{ T}$$

$$B_{c2}(T) = B_{c2}(0) \{1 - (T/9.2)^{1.7}\} \qquad B_{c2}(4.2 \text{ K}) = 10.7 \text{ T}$$

$$T_c(B) = T_c(0) \{1 - (B/14.5)\}^{0.59} \qquad T_c(5 \text{ T}) = 7.16 \text{ K}$$

Similar relations are found for Nb<sub>3</sub>Sn and BSCCO 2212 and 2223.

### Temperature margin, T<sub>cs</sub>

When a transport current flows, the onset of resistance is is further reduced from T<sub>c</sub> to T<sub>cs</sub>, the current sharing temperature

$$T_{cs}(B,I) = T_b + (T_c(B) - T_b) (1 - I/I_c)$$
  $T_{cs}(5 T_r I_c/2 A) = 5.7 \text{ K only!}$ 

- So we lost a lot of margin from 9.2 K  $\rightarrow$  7.2 K  $\rightarrow$  5.7 K versus 4.4 K.
- At 4.4 K, at 50% I<sub>c</sub> and 5 T there is only 1.2 K margin!
- At 75% of I<sub>c</sub> we get 0.7 K, so we never can operate very near to I<sub>c</sub>!
- Following  $\Delta T = Q / c(T)$ , release of energy (heat) from various sources will cause a temperature rise and thus the superconducting state is very seriously in danger.
- The heat that can be absorbed without reaching  $T_{cs}$  is the enthalpy difference  $\Delta H = \int c(T) dT$  between  $T_{cs}$  and  $T_{o}$ .



# Adiabatic Filament Stability, dfil

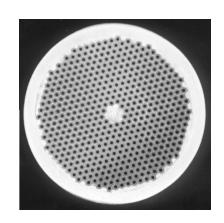
Field penetration in filaments, the Critical State Model

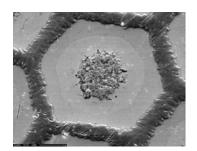
- In the filament magnetic energy is stored
- When disturbed, the heat must be taken up by the enthalpy of the filament
- A disturbance  $\Delta T1$  will cause a  $-\Delta Jc$ , so flux motion, leading to E, this leading to heat and so again a  $\Delta T2$
- When  $\Delta T2 > \Delta T1$ , the process will accelerate and the flux profile collapses
- Based on simple slab model, the adiabatic stability criterion is found:

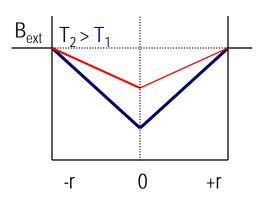
$$d_{fil}$$
.  $J_c < { 3 c (T_c-T_o) / \mu_o }^{1/2}$ 

So we see a maximum filament thickness for a given current density, to guarantee stability.

For NbTi, c=5600 J/m<sup>3</sup>;  $T_c$ (5 T)=7.2 K,  $T_o$ = 4.2 K and  $J_c$  = 3000 A/mm<sup>2</sup>, we find  $d_{fil}$  < 70 μm.







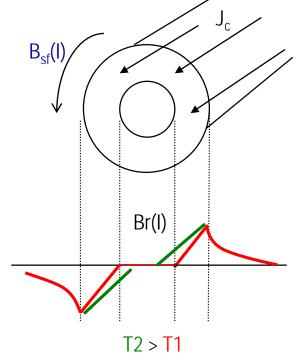


# Adiabatic Wire Self field Stability, Dwire

### Filaments coupled by self field

- Adiabatic filament stability requires fine filaments in a matrix
- These can be de-coupled for transverse fields by twisting
- But are still fully coupled by the self-field
- Again following the CSM, we see the field penetration profile disturbed by a  $\Delta T$
- Field profile has to change, penetrates deeper, causing heat dissipation taken up by the enthalpy up to a certain limit
- Assuming η=sc/total ratio and current density ηJ
- We find for the adiabatic self-field criterion:

$$D_{\text{wire}} \cdot \eta J < \{ 4 \text{ c } (T_c - T_o) / \mu_o \}^{1/2} \text{ f } (I/I_c)$$
  
where f  $(I/I_c) = 1/(-0.5 \ln(I) - 3/8 + i^2/6 - i^4/8)$ 



- So we see a maximum wire diameter for a given Jc and I/I<sub>c</sub>
- Commonly used 0.7 < D<sub>wire</sub> < 1.3 mm in cables.</li>



### Self-field Stability: cable examples

#### ITER cable for central solenoid

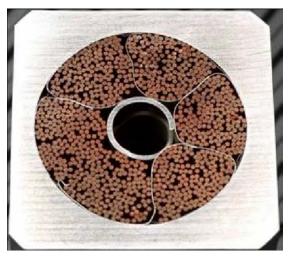
- 65 kA at 13.5 T, ~1152 Nb3Sn wires parallel in a twisted multi-stage cable.
- Cable layout with 5 stages: 1x3x4x4x4x6.
- Wire 0.81 mm, filaments 4 μm.
- The strands take all positions in the cable to guarantee equal current sharing.

### LHC type Nb3Sn Rutherford cable

- 33 stands single stage twisted.
- 13 kA at 11 T.

#### ATLAS cable

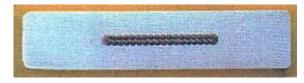
- Al stabilized 40 strands Rutherford cable.
- 65 kA at 5 T.



~1152 wires ITER Nb3Sn cable



33 wires LHC-type Nb3Sn cable



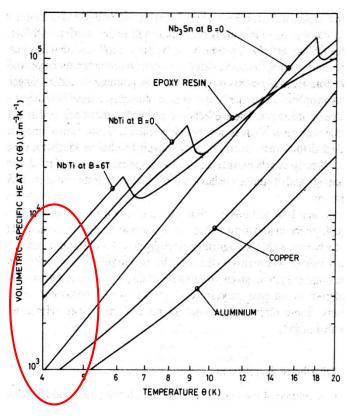
40 strands ATLAS BT cable



### Temperature jumps, low heat capacity

### Why is release of heat so critical at 4 K?

- Heat capacity is strongly T-dependent
- Copper-NbTi composite:
   Cp(T)= η((6.8/η+43.8)T³+(97.4+69.8 B)T)
   μJ/mm³K, at 5 T and 40% NbTi in a Cu matrix:
- 2.5 μJ/mm<sup>3</sup>K at 4.2 K and
- 0.5 μJ/mm³K at 1.9 K!
- 2.5 μJ/mm corresponds to a movement in a 1 mm wire at 5 T, 500 A of 1 μm only!



### Heat release of µJ/mm³ has to be avoided, otherwise magnet will quench

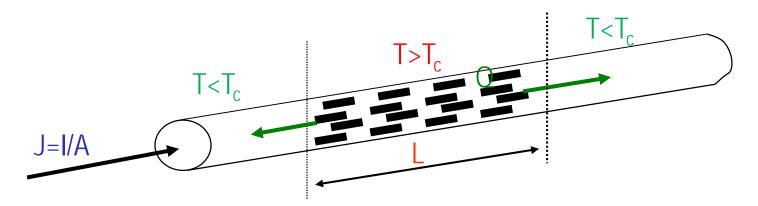
- avoid friction and slip-stick by introducing low friction sliding (Kapton films wrapped around wires and cables)
- avoid any displacement, vacuum impregnation of coils
- avoid resin cracks, avoid local stress concentrations at bonded surfaces.



# Point disturbance, MPZ

### **Minimum Propagation Zone** (1-d case)

- How large must the distortion be to get a quench?
- Consider a wire with current I, heat removal Q along the wire and central zone in normal state (simple, one dimensional case)



Look for length L where heat produced is equal to heat removed:

$$\rho J^2 A L \approx 2 \lambda A (T_c - T_{bath}) / L$$

$$L = \{ 2 \lambda (T_c - T_{bath}) / \rho J^2 \}^{1/2} = MPZ$$

Propagation occurs when L > MPZ and recovery when L < MPZ



# Minimum Propagation Zone, MPZ

### Examples of MPZ in a various wires

In a bare NbTi wire or filament: take 5 T; 3000 A/mm<sup>2</sup>;  $\rho$ = 6x10<sup>-7</sup>  $\Omega$ m;  $\lambda$ = 0.1 W/mK; T<sub>c</sub>= 7 K and we find 0.3  $\mu$ m only, pure NbTi can not be used!

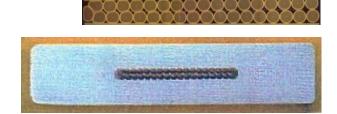


- NbTi with CuNi matrix would give 3 μm and 0.1 μJ!
- Such wire is extremely sensitive to any heat pulse

Remedy: reduce  $\rho$  by using copper matrix (3x10<sup>-10</sup>  $\Omega$ m, factor 2000!) and increase  $\lambda$  by using copper (>200 W/mK, factor 2000 again!)

We see how wonderful copper (or Al) is, without copper no sc magnets!

- $\checkmark$  factor 2000 improvement, from  $\mu m$  to few mm and  $\mu J$  range
- ✓ for a typical LHC cable we get about 15 mm
- ✓ and in the ATLAS conductor (600 mm² pure Al and 20 kA) we get about 500 mm!





# Why magnets need High Current & Cables

Magnetic field and stored energy

 $B \propto N.I$   $E \propto B^2.Volume$ 

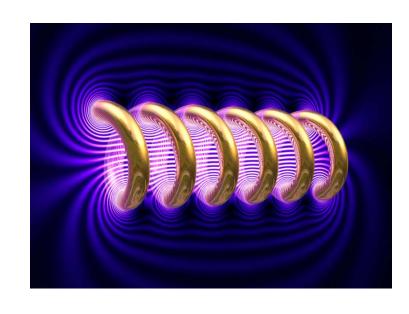
Inductance  $L \propto N^2$ 

- Need safe survival from a quench
- Energy dump within short time before conductor burns out
- → Thus low N, high current I

Also  $I_{safe} \propto J.E/V_d$ , kV-range for  $V_d$ , with usual current densities this leads to 10-100 kA

→ Given common strand currents of 100 to 500 A, we need for large scale magnets multi-strand cables with 20-1000 strands!

No escape!





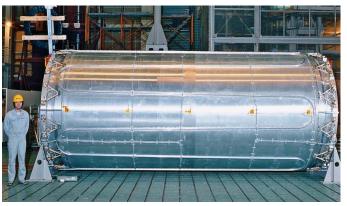
# Scaling: $I_{safe} \propto J \times B^2 \times Volume$



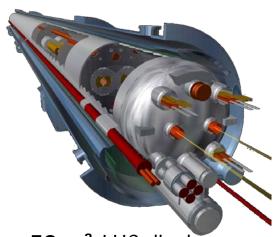
0.0001 m<sup>3</sup> HF insert



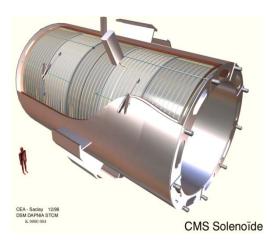
2 m<sup>3</sup> MRI magnet 200-800 A @ 1-3 T, ~10 MJ



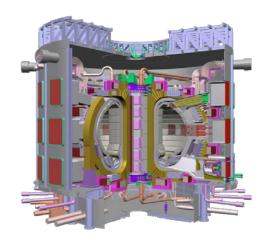
25 m³ ATLAS solenoid 8 kA @ 2T, 40 MJ



50 m<sup>3</sup> LHC dipole 12 kA



**400 m³** HEF detector magnet **20 kA** @ 4 T, 2.6 GJ



**1000 m<sup>3</sup>** ITER magnets **40-70 kA** @ 10-13T, 50 GJ



### Request for: high current conductors

200 A HTS tape?

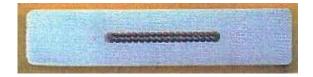
**-22**(1) 11 11 11 11 12 12 12

Single: No!

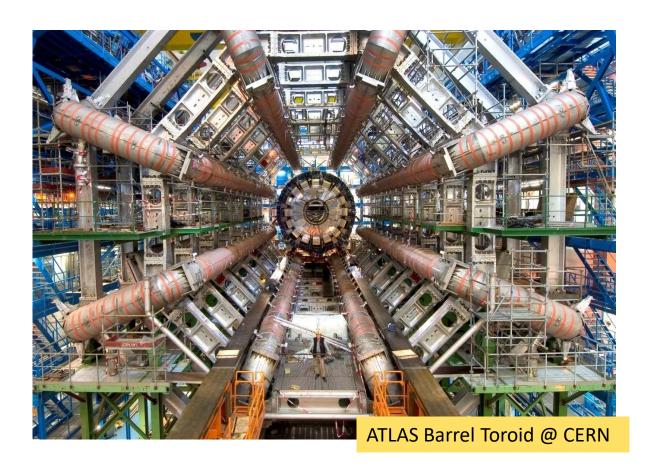
Cabled: may be, but

to be developed

65000 A@5T Al-NbTi/Cu?



Yes!



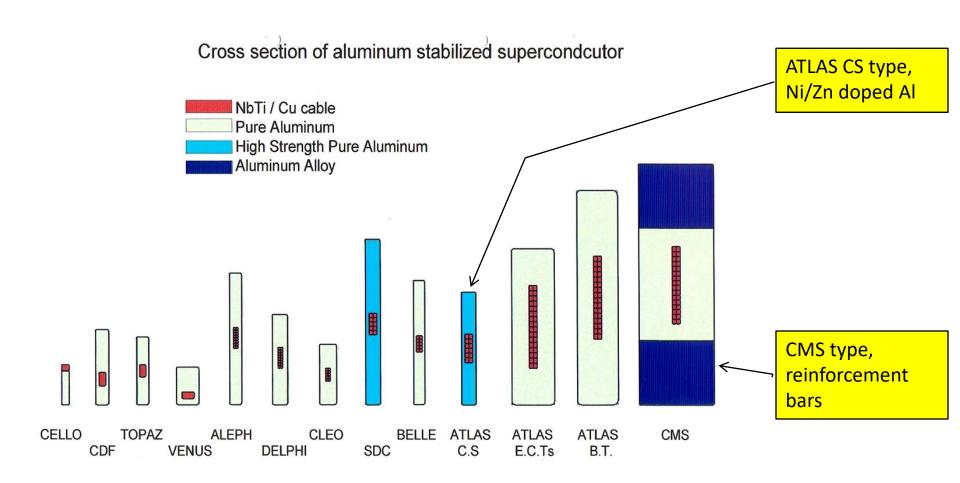
One can not build large scale magnets from single wires or tapes.

We need superconductors that can be cabled and survive a quench!



# **Novel Detector Magnet Superconductors**

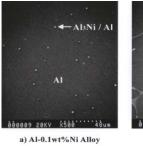
For the next generation detector magnets, conductors are further developed and reinforced, more stored energy, larger size.

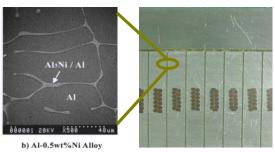




### Re-inforcing Al-stabilized conductors

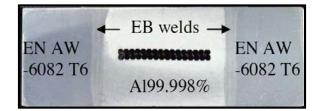
- Option 1
   Ni or Zn doped Aluminum
- Used in the ATLAS Solenoid mechanical reinforcement while keeping quench stability.







- Option 2
   Reinforce with Al-alloy side bars,
   EB- welded to the Al and NbTi/Cu co-extruded conductor
- Doable but expensive.

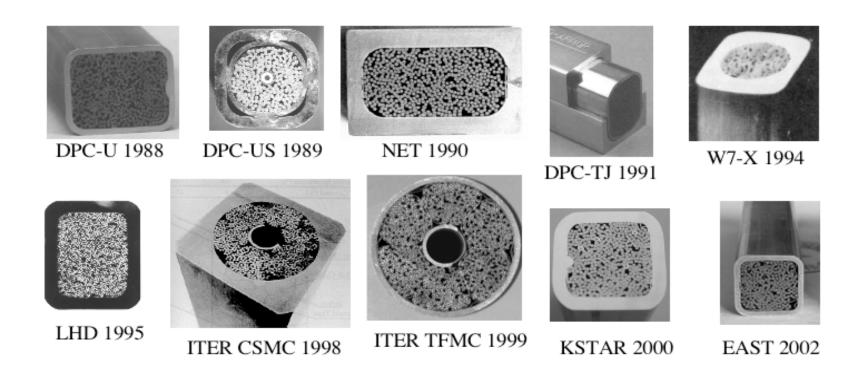






### Alternative: use a Cable-in-Conduit

More than 25 years cable-in-conduit conductors (CICC) are in use for fusion magnets with forced flow helium maximizing heat removal and stability.



Very flexible in choosing cable size, current rating, strength and helium cooling directly on the superconductor → maximum stability

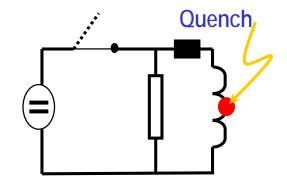


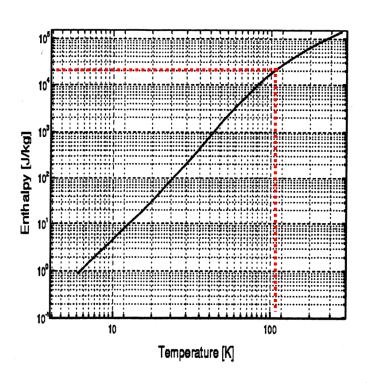
### Stored energy to dump

The energy stored in a magnet is  $W_L = \frac{1}{2} L I^2 [J] = \frac{1}{2} \int BH \ dV,$  the energy density being ½ BH or  $B^2/2\mu_o$ 

This energy could be absorbed by the magnet cold mass assuming a safe temperature  $T_m$ 

- $W_L/m = \int_0^{Tm} C_p(T) dT = H(T_m) H(T_o = 4.2)$  $\approx H(T_m)$  since  $C_p(4.2)$  is negligible
- For 150 K, we can absorb about 20 kJ/kg cold mass provided uniformly distributed
- Usual values for W<sub>L</sub>/m are in the range
   <10 kJ/kg, so apparently no problem</li>
- But heat distribution must be controlling the normal zone spatial distribution and speed.







### Adiabatic heating of the conductor

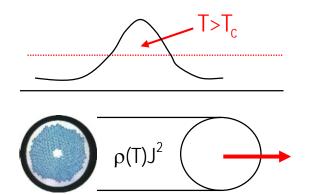
#### Temperature of the conductor?

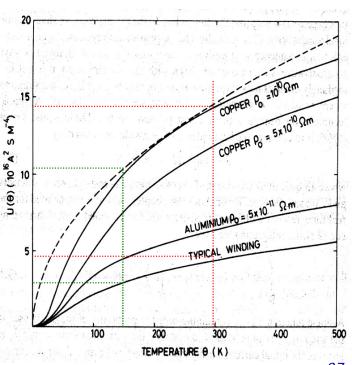
• Heating in the normal zone  $\rho J^2$  is taken up by the conductor enthalpy:

$$\rho(T) J^2(t) dt = c(T) dT$$

$$_{o}\int_{0}^{t}J^{2}(t) dt = _{4}\int_{0}^{T}c(T)/\rho(T)dT = constant = F(T_{m})$$

- F is the Load Integral, used to assess transient thermal loads in devices.
- F is a constant, calculated for NbTi, Cu, resin and any mixture as a winding.
- Typical values for F(T<sub>m</sub>) are in the range 2-9x10<sup>16</sup> for 150 K and 5-15 for 300 K maximum temperature depending on the conductor composition.







### Adiabatic hot spot temperature

$$_{0}\int_{0}^{t}J^{2}(t) dt = _{4}\int_{0}^{T}c(T) / \rho(T) dT = constant = F(T_{m})$$

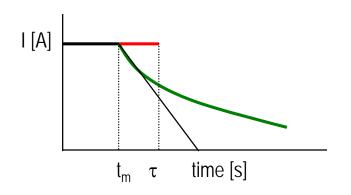
Simple solutions exist for constant or exponential decaying currents

Constant current

$$J^2 t_m = F(T_m) \rightarrow t_m < F/J^2$$

Exponential decay

$$J^2 \tau /2 = F(T_m) \rightarrow \tau < 2F/J^2$$



#### Examples

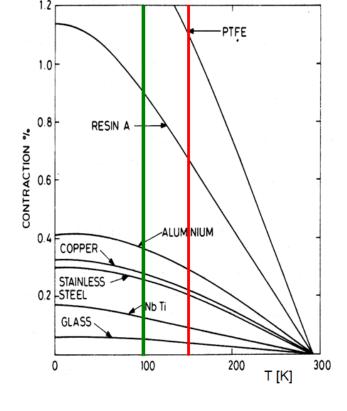
- NbTi/Cu and CuNi matrix conductors with J = 500 A/mm<sup>2</sup>
- $F(300) \propto 1/\rho$
- F(300) for Cu is  $\sim 1.4 \cdot 10^{17}$  and  $\sim 1.4 \cdot 10^{16}$  for CuNi (or pure NbTi)
- Maximum τ in NbTi/Cu before reaching 300 K is a 0.1-1 second
- Maximum  $\tau$  in NbTi or NbTi/CuNi is ~ms, so very little time to react and the conductor will burn out when used at high current density!



### Safe hot spot temperature

#### Criterion for hot spot temperature

- Beyond 900 K Al structures start to collapse.
- Beyond 650 K we start to lose pinning, so J<sub>c</sub>.
- Even 300 K is too high, as it endangers the windings.
- Severe thermal shock due to differential thermal contractions will occur.
- This may cause resin cracking and de-bonding, and thus training or degradation.
- ✓ A "safe" hot spot temperature is 100-150 K!
- Usually 100 K is taken nominally and a peak of 200-300 K for exceptional cases (failing protection systems for example).



 300 K may be acceptable for an R&D magnet, but is not an acceptable design value for a detector magnet that has to survive, operate at minimum risk and must be quench-recovered within 3-4 days.



#### Destructive power of uncontrolled quenches

LHC dipole of 15m and 8.35T stores 8 MJ, which corresponds to melting 1.5L of copper, enough to evaporate 10cm of coil!

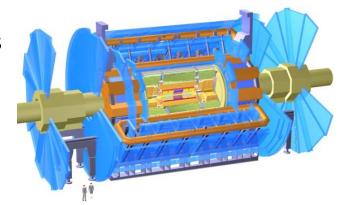
And we have seen in Sep 2008 what a few magnet quenches can do!

ATLAS detector toroid stores 1.6 GJ, good for 600L of melted copper, or equivalent to the collision energy of 100 trucks of 40 tons with speed of 100 km/h!

To be safe with equipment and personnel: Quench Protection has to cover all possible quenches in the entire electrical circuit from + to – terminal on the cryostat (current leads & bus connections & coil).



Damage at an LHC interconnect

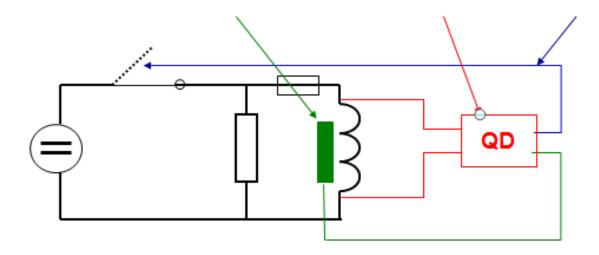




#### **Quench Detection**

#### Quench detection circuit

- The magnet safety system comprises the quench detectors, logics for opening switches and to supply current to the quench heaters.
- The system must be extremely reliable and power secured.
- ✓ The motto is: "keep it simple", meaning robust and straight forward detection circuits, simple electronics, hardwired and 3-5 times redundant.
- First the quench, a normal zone, must be detected, then switches have to be opened and quench heaters activated.





#### **Quench detection methods**

#### Bridge method

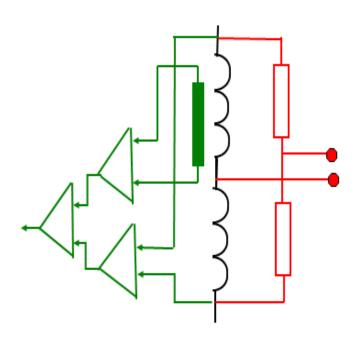
- Detects the resistance in any branch of the coils, very robust, simple and proven.
- 3 sets of bridges, asymmetrically connected to see symmetric quenches.
- Commonly used for large magnets.

#### Voltage across coil

 Voltage across coil compensated for the inductive component. Requires differential amplifiers, more complicated, more electronics.

#### Other methods

- Temperature, pressure gages, pick-up coils, strain sensor, etc.
- Many proposed, but mostly not used.

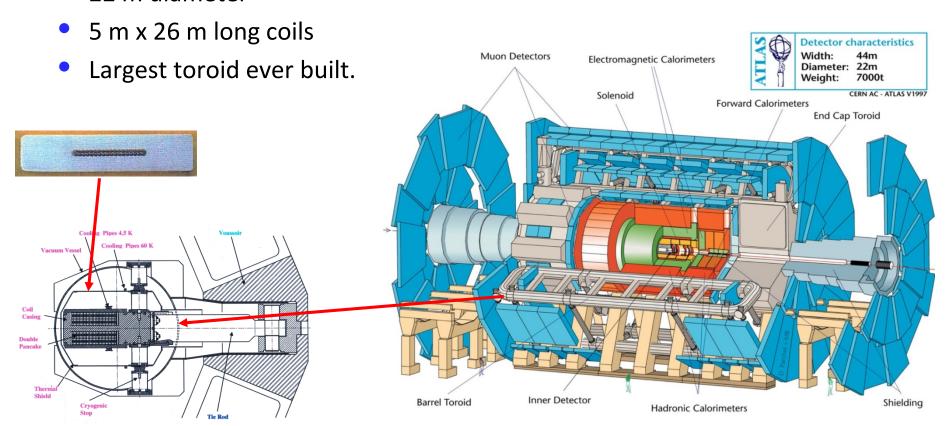




### **Example ATLAS Toroids**

#### Toroids quench detection:

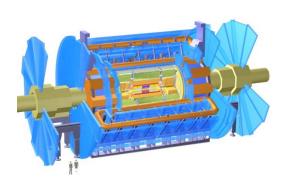
- 1.5 GJ energy, 20 kA current, 4 T peak field, 3 kJ/kg stored
- 3 toroids, each comprising 8 flat coils, thermally not connected
- 22 m diameter

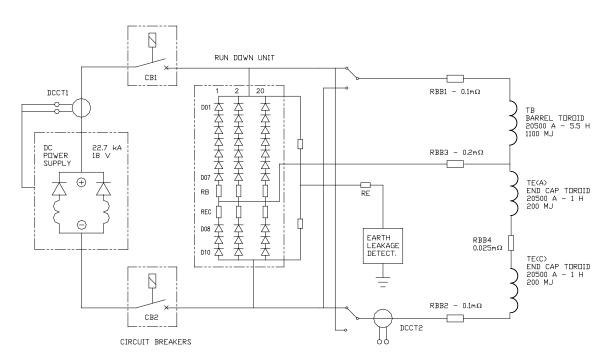




### **Example ATLAS Toroids**

- All toroids 3 x 8 = 24 coils are connected in series.
- The energy is dumped in the 3 toroid cold masses, voltage limited to 40V.
- Quench detection by 3 bridges + 3 differential units per toroid so 6 fold redundancy, heaters are fired introducing 4 normal zones in every coil, expected maximum hot spot temperature ~100K.
- Threshold 0.3 V
- Low pass filter 1 s
- Fast dump in about 80 s.



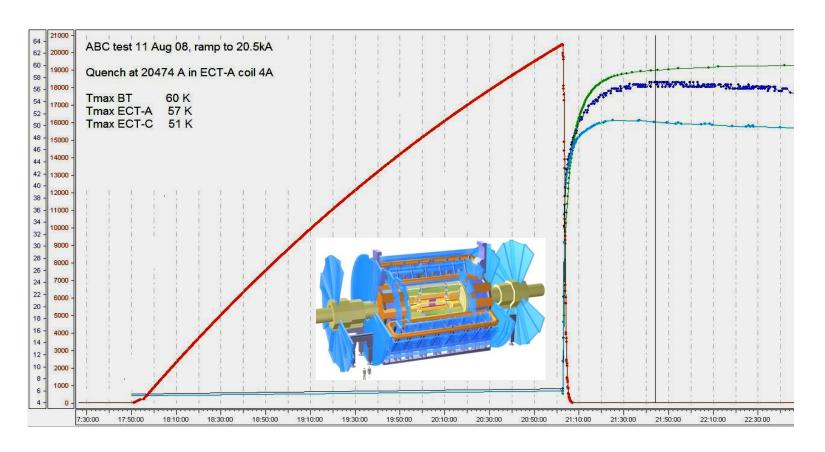


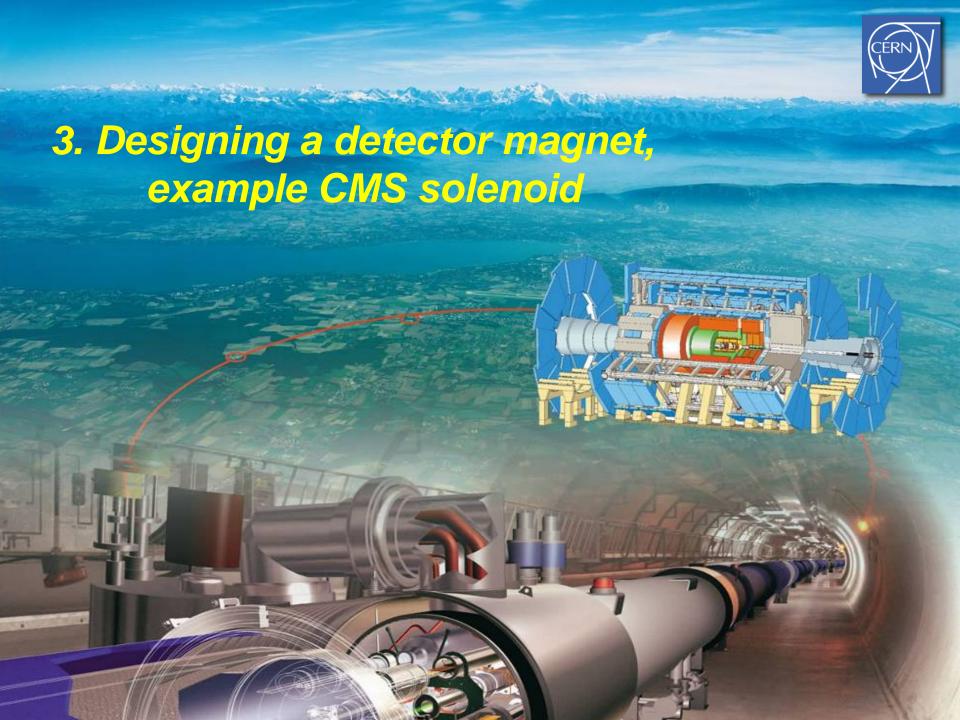


### **Example ATLAS Toroids**

#### Toroid Fast Dump test result:

- Provoked Quenches at 20.5 kA, heaters fired, quench is spread
- ~ 60 K cold mass temperature at 20.5 kA, recovery in about 80 hours
- $^{ullet}$   $^{\sim}$  90 K hot spot in the conductor, perfectly safe quench behavior.

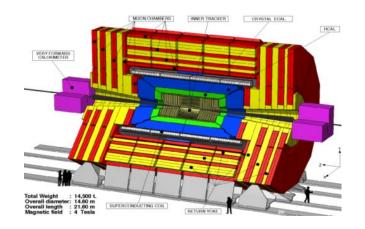






### Design steps: example CMS solenoid

- 1. Magnetic field calculation
- 2. Effect of the iron yoke
- 3. Magnetic stored energy
- 4. Lorentz forces in the coils
- 5. Hoop stress
- 6. Choosing current vs self-inductance
- 7. Conductor dimensions and layers
- 8. Conductor details
- 9. Stabilizer, Cu or Al





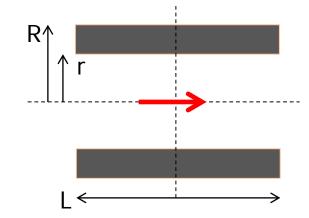


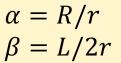
#### Design steps: Magnetic field, no iron

#### Field calculation without iron yoke:

Current density: 
$$J = {^{NI}}/_{L(b-a)}$$

Field 
$$B_o = Jr\mu_o\beta \left\{ \frac{\alpha + \sqrt{(\alpha^2 + \beta^2)}}{1 + \sqrt{1 + \beta^2}} \right\}$$
  
 $B_o = \mu_o nI \text{ for } \beta \to \infty$ 



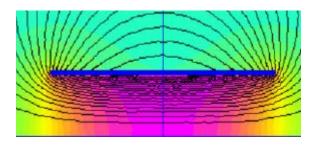


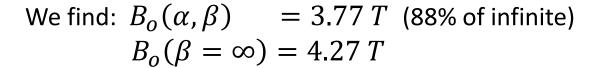
N turns I current n= N/L

#### With real CMS magnet sizes:

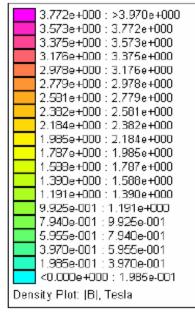
 $L = 12500 \, mm$ 

N = 2180; I = 19500 A





With a FEM code we find 3.77 T as well.



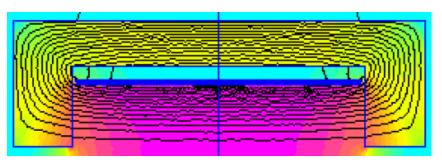


### Design steps: Magnetic field, with iron

Accurate analytical formulae do not exist, a calculation with a FEM code is needed (OPERA-3D, ANSYS, COMSOL).

Simple solid magnetic yoke:

$$B_o = 4.17 T$$
 (98% of infinite)

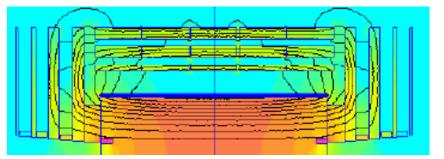


Iron is a magnetic mirror, the coil is almost infinite.

Real iron with gaps for detectors:

 $B_0 = 4.0 \text{ T in center}$ 

4.6 T in conductor



#### Stored energy:

FEM calculation yields:  $\frac{1}{2\mu_0} \int B^2(r,z) dV = 2.6 \ GJ$ 

Simple approximation:  $\frac{1}{2\mu_0} B^2 V = 2.46 \text{ GJ}$ , V = bore volume

1.944e+000 : 2.160e+000 1.728e+000 : 1.944e+000 1.512e+000 : 1.728e+000 1.296e+000 : 1.512e+000 1.080e+000 : 1.296e+000 8.642e-001 : 1.080e+000 5.481e-001 : B.542e-001 4.321e-001 : 6.481e-001 2.161e-001 : 4.321e-001 <7.652e-005:2.161e-001 4.685e+000 : >4.932e+000 4,438e+000 : 4,685e+000 4.192e+000 : 4.438e+000 3.945e+000 : 4.192e+000 3.699e+000 : 3.945e+000. 3.452e+000 : 3.699e+000 3,206e+000 : 3,452e+000. 2.9<del>5</del>9e+000 : 3.206e+000 2.712e+000 : 2.959e+000 2.465e+000 : 2.712e+000 2.219e+000 : 2.466e+000 1.973e+000 : 2.219e+000 1.726e+000 : 1.973e+000 1.479e+000 : 1.726e+000 1.233e+000 : 1.479e+000 9.863e-001 : 1.233e+000 .397e-001 : 9.863e-001 4.932e-001 : 7.397e-001 2,466e-001 : 4,932e-001 <0.000e+000 : 2.466e-001

4.104e+000 : >4.320e+000

3.888e+000 : 4.104e+000 3.672e+000 : 3.888e+000

3,456e+000 : 3,672e+000 3,240e+000 : 3,456e+000 3,024e+000 : 3,240e+000

2.808e+000 : 3.024e+000 2.592e+000 : 2.808e+000

2.376e+000 : 2.592e+000 2.160e+000 : 2.376e+000



## Design steps: Magnetic forces

Lorentz forces due to B and J cause axial compressive forces and radial forces causing hoop stress:

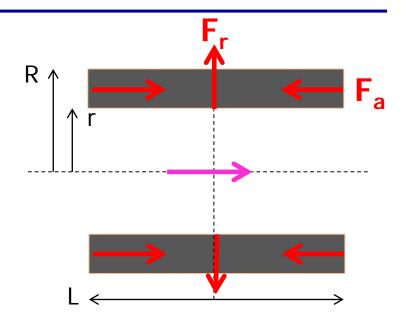
$$\overline{F} = \int (\overline{J} x \overline{B}) dV$$

- Radial field causes axial force F<sub>a</sub>
- Axial field causes radial forces F<sub>r</sub>
- In fact the solenoid wants to blow up into a ball shape

For CMS: 
$$F_a = +1.66 \text{ GN}$$
,  
 $F_r = -140 \text{ MN } (14 \text{ kt})$ 

The "Ball" Pressure  $\approx$  F<sub>r</sub>/surface = 6.6 MPa

- Magnetic pressure =  ${}^{B^2}/_{2\mu_0} = 6.4 MPa$
- or 64 atm







### Design steps: Hoop stress, coil thickness

The radial pressure is reacted in the cylinder with thickness t (windings + extra material) by the hoop stress:

$$\sigma_{hoop} = {^{aP_r}/_t}$$

To be respected design rule:

$$\sigma_{hoop,max} = \frac{2}{3} \rho_{yield}$$

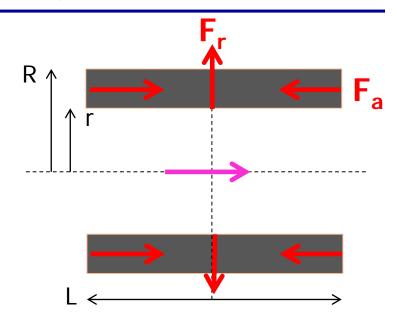
Structural coil thickness:

$$t = {3 \, r \, P_r \over 2 \, \rho_{yield}} = 320 \, mm$$
,

using 100 MPa annealed Al5083, or

t = 190 mm, based on special 170 MPa Al5083-H321.

→ So we need some 190 - 320 mm thick structural special Al alloy on top of the soft conductor to withstand the radial forces in a safe way.







### Design steps: Current vs self-inductance

Self-inductance L<sub>c</sub> and current I are linked through the stored energy:

$$E = \frac{L_c I^2}{2} = \frac{1}{2\mu_o} \int B^2 dV \approx \frac{1}{2\mu_o} B_o^2 V$$
, and  $L_c = \mu_o N^2 \pi r^2 2/L$ 

- Current I must be high for protection reasons, say 20 kA
- Then  $L_c \approx 14$  H and for N follows N  $\approx 2100$ .
- Adaptation to conductor & coil dimensions leads to 19.5 kA / 2180 turns.
- The coil has 42.5 10<sup>6</sup> ampere-turns.

In the windings section of

≈ 320 mm x 12500 mm we have to put in place:



- 2180 turns of superconducting cable with 19.5 kA
- extra stabilizing and quench protection material around the cable
- conductor insulation
- structural reinforcement for handling the hoop stress
- an outer support cylinder for integrity and conduction cooling supply.



### Design steps: Conductor size and layers

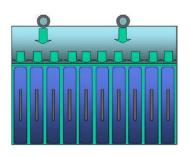
#### 4 T is made with 2180 turns and 19.5 kA current, but:

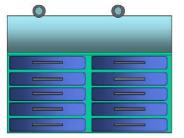
How many layers is wise?

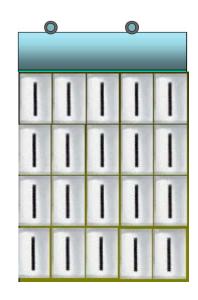
- Coil winding section is 12500 mm x 263 mm,
- n layers x conductor height = 263 mm
- Use 1 (easy), or even number of layers: 2, 4 or 6
- 1 or 2 layers requires a too thin conductor to be wound on its small edge.
- Then 4 layers is best, few layers only and acceptable conductor size of 66 x 23 mm<sup>2</sup>, 6 layers would mean 44 x 34, almost square.

#### There is a thermal argument as well:

• winding on small-edge gives less layers, so less thick insulation (resin, glass, polyimide) between the superconductor (NbTi) and the heat sink (cooling pipe), thus a small temperature gradient.





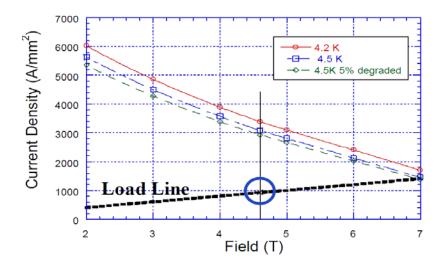




#### Design steps: Superconductor needed

The coil runs at 19.5 kA with a peak field of 4.6 T at 4.5 K:

- Critical current density at 4.6 T/4.5K including 5% cabling degradation is 3000 A/mm<sup>2</sup>.
- We need margin so we run at 1/3 of the critical current, at 1000 A/mm<sup>2</sup>.



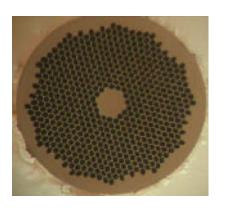
- 19500 A and 1000 A/mm<sup>2</sup>,  $\rightarrow$  need 19.5 A/mm<sup>2</sup> sc per turn=cable
- Self-field stability → wire diameter <1.28 mm</li>
- A minimum Cu/sc ratio is  $1:1/1 \rightarrow Asc = 0.61 \text{ mm}^2$
- Number of strands in the cable is then 19.5/0.61 = 32.
- Filament size? Adiabatic filament stability requires <40 μm.
- The filament section is 0.00126 mm<sup>2</sup>  $\rightarrow$  we need  $\geq$ 484 filaments.
- Twist pitches on strand a cables can be standard giving a good cable stability as needed for the cable/Al co-extrusion process.
- Thus Ls=25 mm and Lc= 185 mm and twist directions SZ.



# Design steps: wire & cable specification

Rutherford cable

Following these arguments the cable specification is now as follows:







Strand Constituents	Material	
High homogeneity Nb-Ti	Nb 47±1 W t % Ti	
High Purity Copper	RRR > 300	
Niobium Barrier	Reactor Grade I	
Strand Design Parameters	Parameters	
Strand Diameter	$1.280 \pm 0.005 \text{ mm}$	
(Cu+Barrier)/Nb-Ti ratio	$1.1 \pm 0.1$	
Filament diameter (mm)	< 40	
Number of Filaments	• 552	
Strand Unit length (m)	2750	
Twist Pitch	$45 \pm 5 \text{ mm Z (RHS)}$	
Strand Minimum Critical Current Ic (A)	1925	
(Criteria : 5 T, 4.2 K, 10 μV/m)		
n-value 5T	>40	
Final copper RRR	>100	

Cabling direction
Nominal current
Critical current at 5T, 4.2K
Critical temperature at 4.6T
Current sharing temperature at 4.6T and 19.5 kA

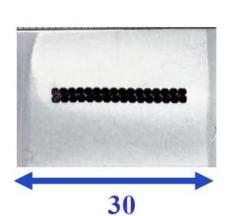
Current sharing temperature at 4.6T and 19.5 kA	≥6.33	K
strand number	32	
dimensions	20.68x2.34	$mm^2$
Cable transposition pitch	185	mm
Cable compacting ratio	87	%

19500 A ≥56000 A 7.35 K



# Design steps: Cable - Al co-extrusion

The cable is co-extruded with high purity Al (RRR>1500)











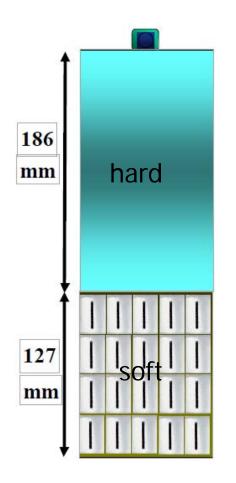




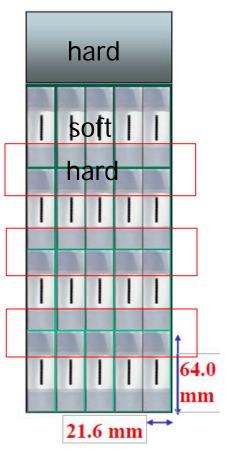
### Coil windings: build up

Now we have: 4 layers of a soft conductor Al/NbTi/Cu, 127 mm thick and a thick support cylinder of 186 mm.

Is this thermally and mechanically an optimal design? No!



- High shear stress at interface
- In the 4 layers, axial forces up to 1400 MN gives 55 MPa in the pure Al >> 20 MPa, not possible.
- Soft 4 layers of 127mm +186mm gives 22
   MPa, is acceptable but strain and shear stress is not uniform.
- A much better solution is to mix soft Al stabilizer and harder Al-alloy support.
- Cure: slice up the thick support cylinder and redistribute it as reinforcement bars on the conductor, creating force bridges in the winding pack in axial direction.

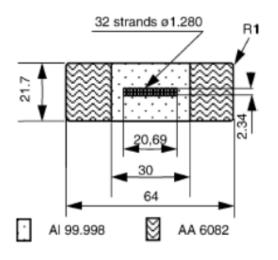


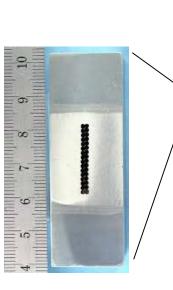


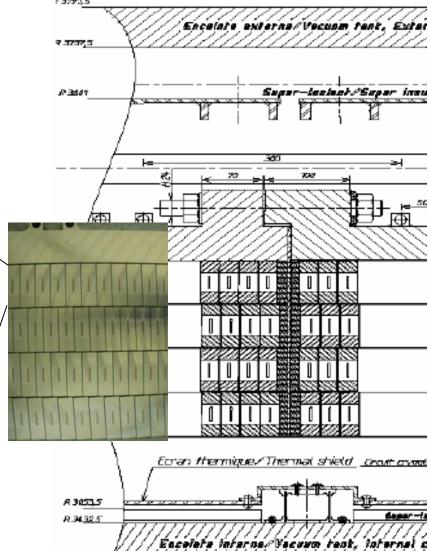
#### Real coil: final solution

Conductor: soft Al-NbTi with NbTi cable reinforced with Al 6082 bars connected by electron beam welding

New yield stress is about 250 MPa!







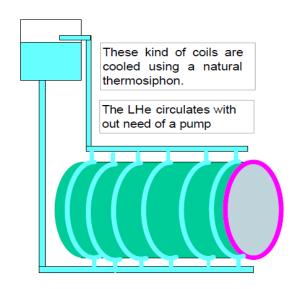


### Making of CMS Solenoid: support cylinder

The CMS magnet cold mass was made in 5 units mostly at ASG – Genua, transported to CERN for on-surface assembly and then insertion as a whole in the CMS cavern.



Support cylinder manufacturing, 5 units





Thermal siphon cooling layout, pipework welded to the cylinder



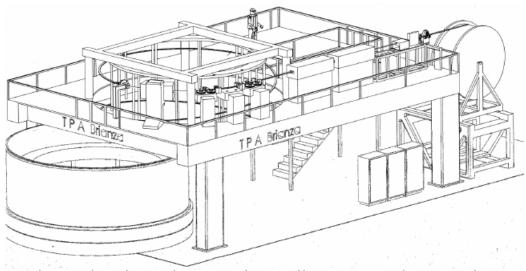
# Making of CMS Solenoid: coil winding



Bend conductor pressed against cylinder



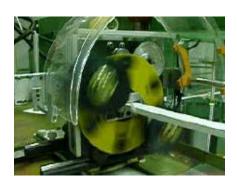
Conductor spiral leading into cylinder



Dedicated coil winding machine allowing winding inside the support cylinder (6.2 m diameter)



Conductor bending



Taping insulation on conductor



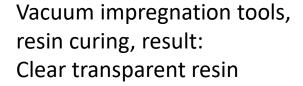
# Making of CMS Solenoid: vac impregnation













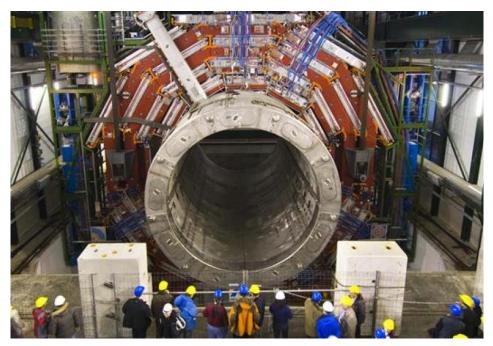




### Making of CMS Solenoid: assembly on site



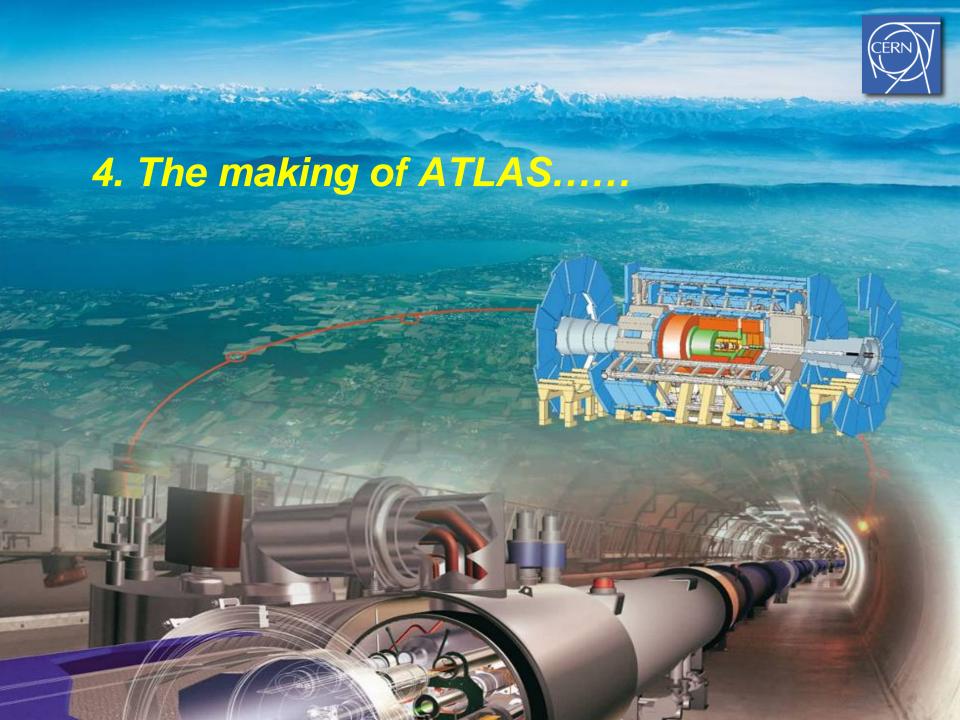






Modules transport, stacking, integration in cryostat and finished coil ready for insertion in cavern.

READY!





#### ATLAS on surface and underground



Underground cavern at - 90 m

 2 shafts give access to a 50,000 m<sup>3</sup> cavern for the detector

Cavern length = 55 mwidth = 32 m

height = 35 m



#### ATLAS sc magnet system

#### 1 Barrel Toroid, 2 End Cap Toroids and 1 Central Solenoid

4 magnets provide 2 T magnetic field for the inner detector (solenoid) and ~1 T for the muon detectors in blue (toroids)

20 m diameter x 25 m long

8300 m<sup>3</sup> volume with field

170 t superconductor

700 t cold mass

1320 t magnets

7000 t detector

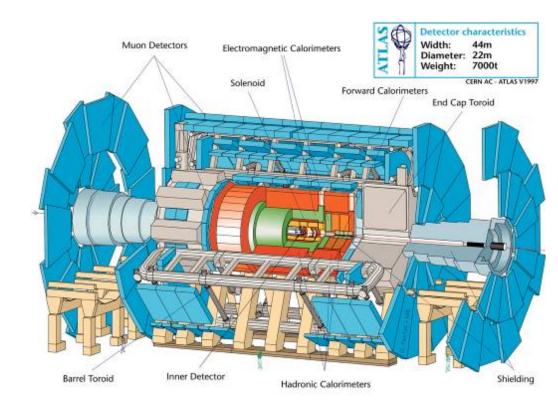
90 km superconductor

20.5 kA at 4.1 T

1.6 GJ stored energy

4.7 K conduction cooled

9 yrs of construction 98-07

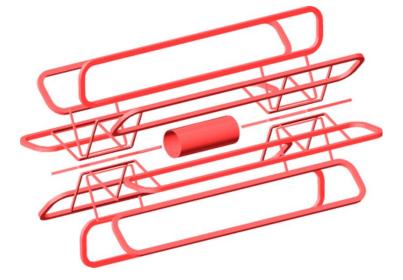


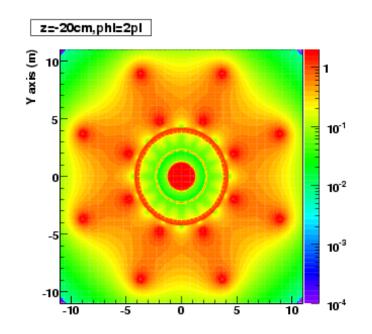
So far the largest trio of toroids ever built

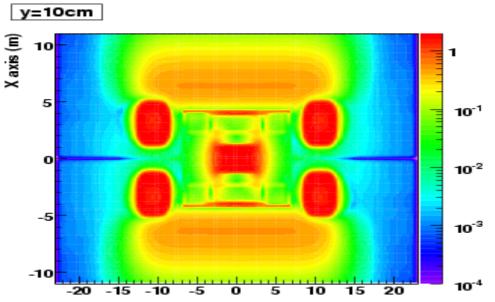


### Magnetic field configuration

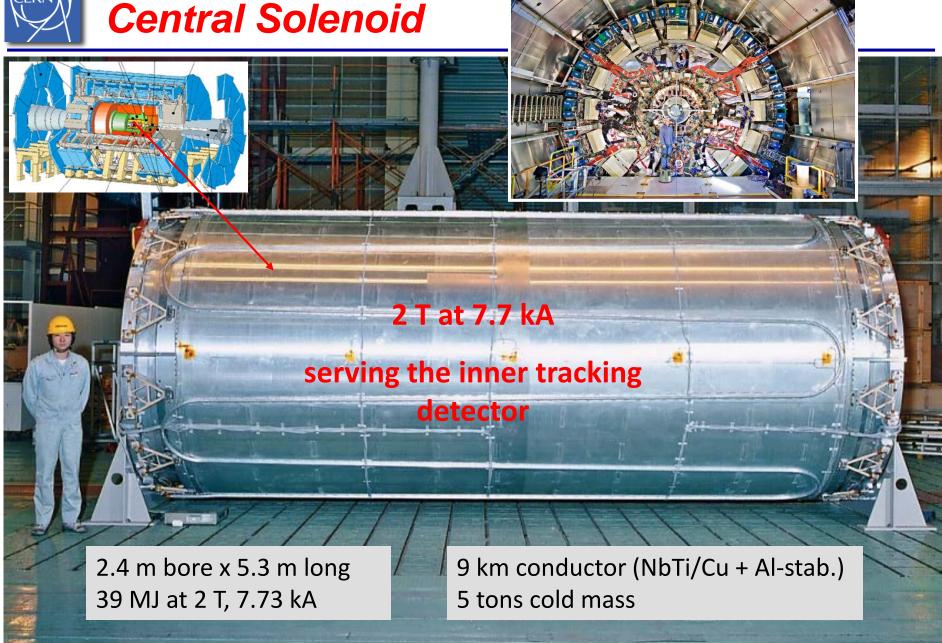
- 2 T in Solenoid closed via return yoke
  - 2.6 T peak in windings
- ~ 0.8 T average in Barrel Toroid torus
  - 3.9 T peak in windings
- ~ 1.3 T average in End Cap Toroid
  - 4.1 T peak in windings









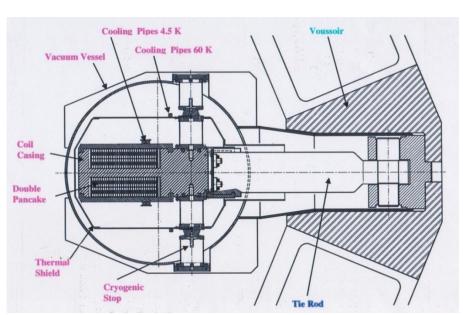




### ATLAS Barrel Toroid Integration

# Construction of a single coil, 8 of these constitute the toroid

- Two racetrack double pancakes
- 2 x 60 turns, pre-stressed and glued in an Al 5083 casing
- Forced flow indirect cooling via redundant circuits of Al 1050 alloy tubes glued on the casing
- Al alloy thermal shield panels
- Superinsulation
- 8 Ti Tie rods
- 16 fre lateral supports
- Instrumentation
- SS vacuum vessel
- Al-alloy warm structure





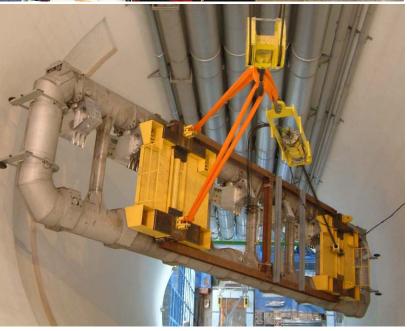
### ATLAS: manufacturing the parts





## ATLAS: Start of Barrel Toroid assembly



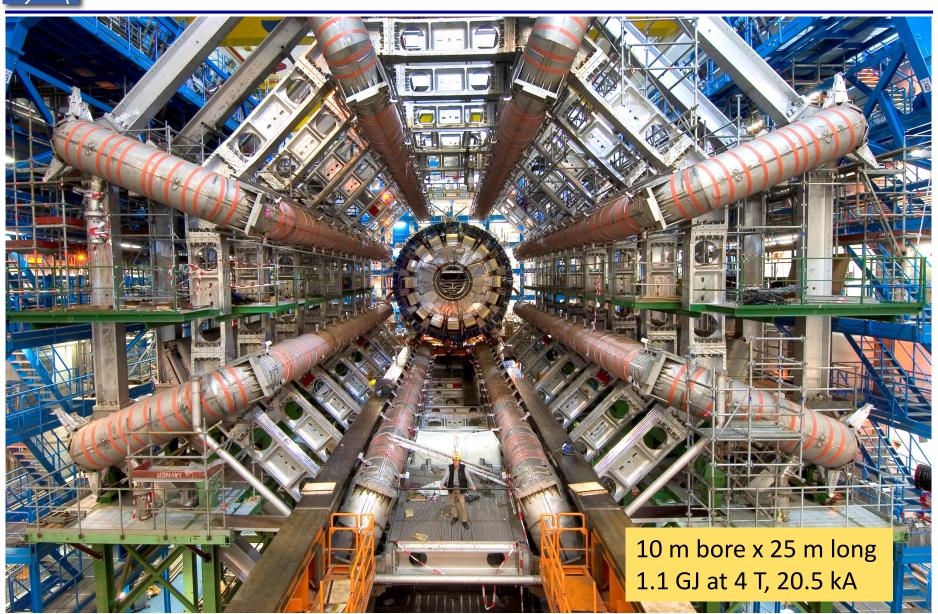




- Transport, decent, reception
- Complex but safe manipulations
- Lowering using 2 lifting frames
- Hydraulic winch with load capacity 190 t

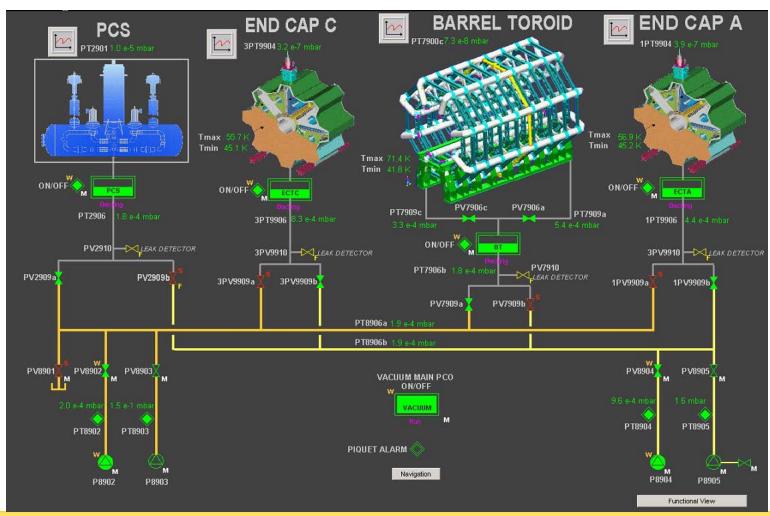


# ATLAS: Barrel Toroid in cavern (Nov 05)





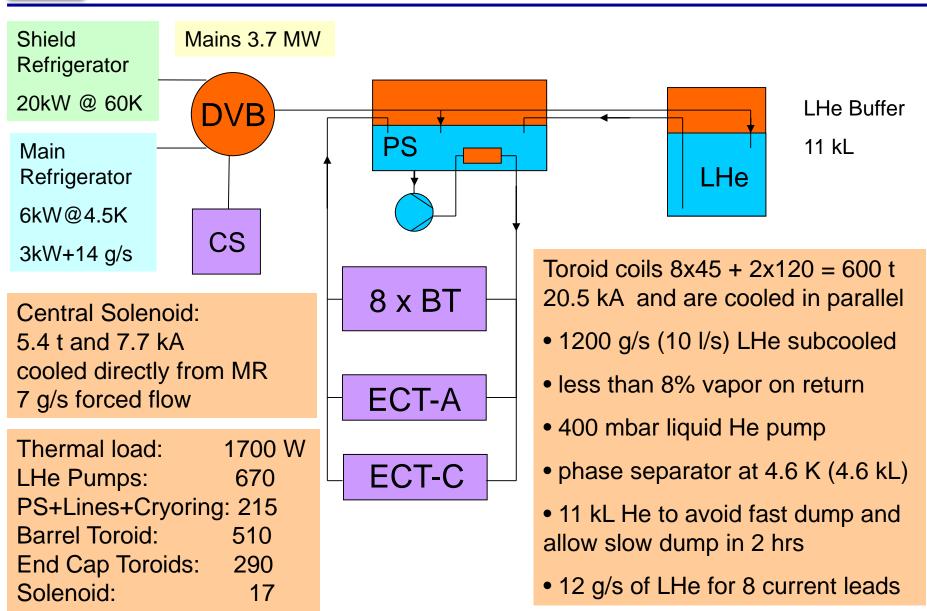
#### Magnet system services: isolation vacuum



- 4 backing pumps, 21 diffusion pumps, stops when no water cooling and power
- must run 24/7, on UPS & diesel, redundant water cooling circuits

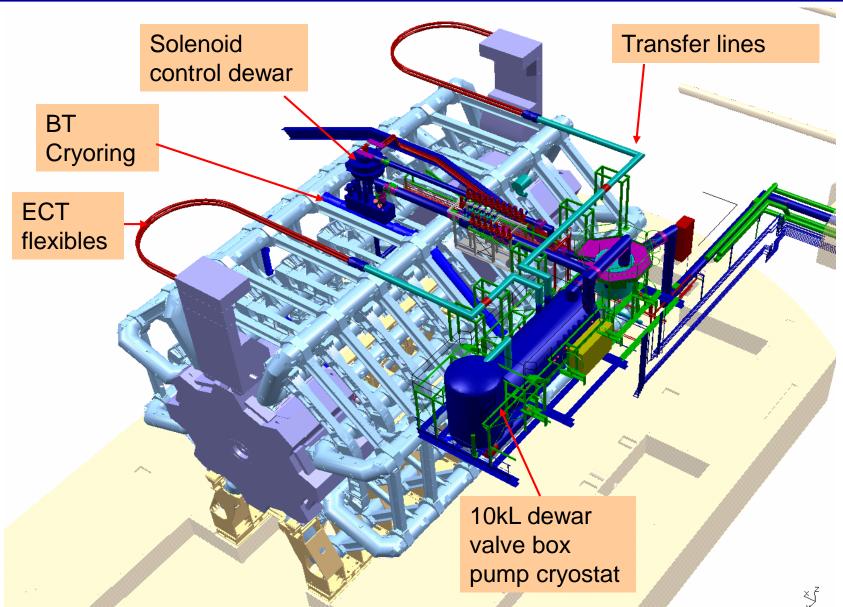


# Magnet services: helium cryogenics



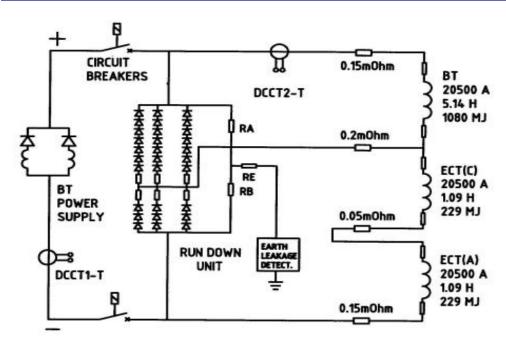


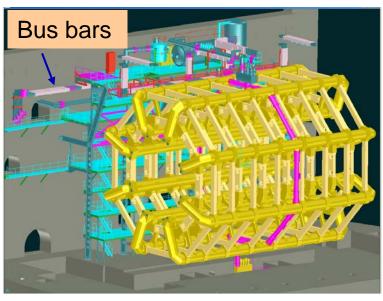
# ATLAS: He proximity cryogenics





### Magnet services: current, 20.4 kA - 18 V





#### **Toroids in series:**

- dump in parallel
- power convertor
- 2 switches
- dump resistors
- diode units
- 240 m Al bus bars

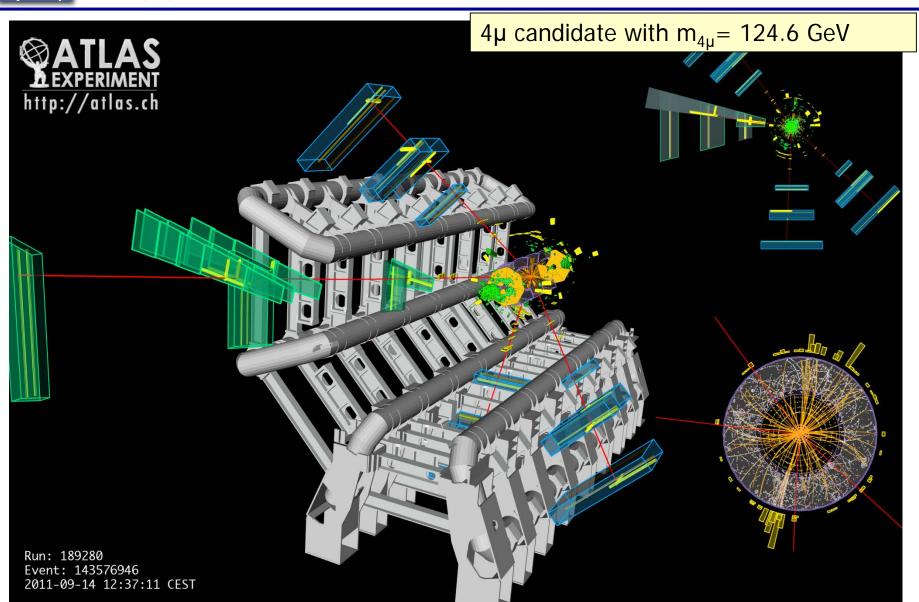






## Higgs events

### $H \rightarrow ZZ^{(*)} \rightarrow 4I$ (4e, 4 $\mu$ , 2e2 $\mu$ )







### It takes time..... Mr Higgs

VOLUME 13, NUMBER 16

PHYSICAL REVIEW LETTERS

19 October 1964

#### BROKEN SYMMETRIES AND THE MASSES OF GAUGE BOSONS

Peter W. Higgs

Tait Institute of Mathematical Physics, University of Edinburgh, Edinburgh, Scotland (Received 31 August 1964)





#### Physics Letters B

Volume 716, Issue 1, 17 September 2012, Pages 1-29



Observation of a new particle in the search for the Standard Model Higgs boson with the ATLAS detector at the LHC  $\dot{\approx}$ 

Universally Available



"I certainly had no idea it would happen in my lifetime at the beginning, more than 40 years ago.

I think it shows amazing dedication by the young people involved with these colossal collaborations to persist in this way, on what is a really a very difficult task.

I congratulate them."

Peter Higgs, July 4<sup>th</sup>, 2012



# 5. Detector Magnets for a 100 TeV p-p collider





## Options for increasing colliding energy

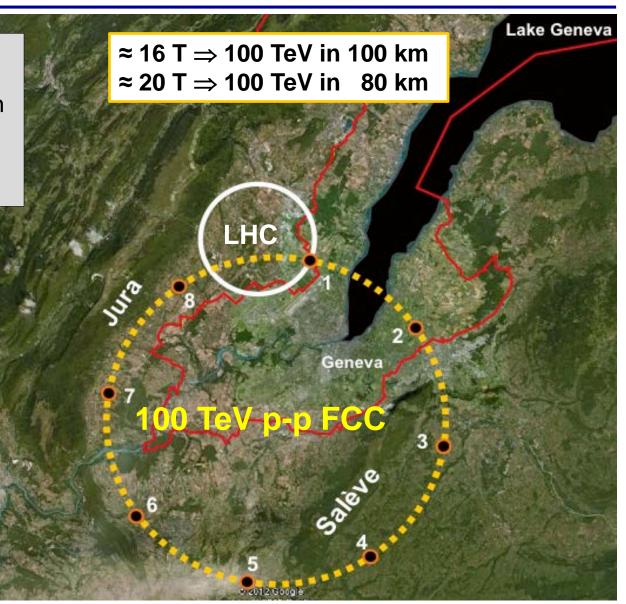
Energy =  $0.3 \times B \times R$ 

B: 1.8 x from NbTi to Nb<sub>3</sub>Sn

**B:** 2.4 x from NbTi to HTS

R: 4-5 x more magnets

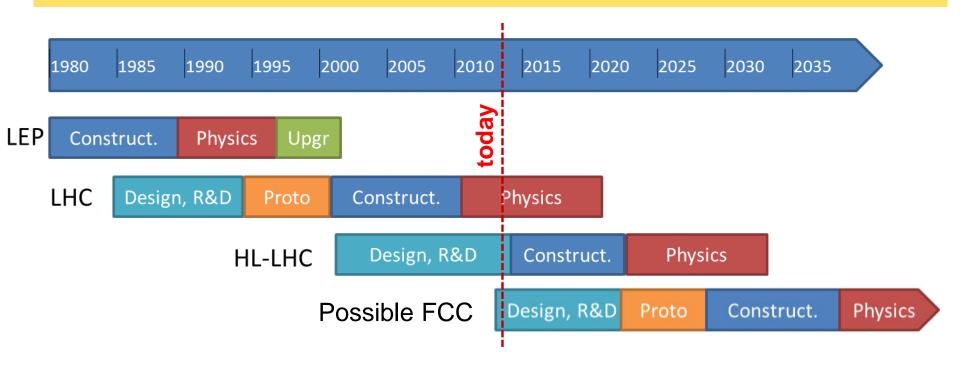
- New 80-100 km tunnel in Geneva area
- pp-collider (VHE-LHC) defining the size
- Options for adding an e+e collider (TLEP) p-e collider (VLHeC)
- CERN-hosted study with international collaboration





### It easily takes 30 years time..... start now

"CERN should undertake design studies for accelerator projects in a global context, with emphasis on **proton-proton** and electron-positron **high-energy frontier machines."** 



FCC Study: p-p towards 100 TeV. Study in progress sine mid-February 2014.

**Leading to Conceptual Design Report by ed of 2018** 

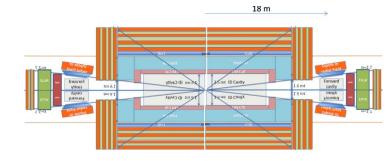


# Design drivers for detector magnets

Bending power: 100 TeV, a 7 x higher collision energy than 14 TeV of present LHC

Same tracking resolution?

$$\frac{\sigma(p_T)}{p_T} = \frac{\sigma(\kappa)}{\kappa} = \frac{\sigma_x \cdot p_T}{0.3BL^2} \sqrt{\frac{720}{(N+4)}}$$



### $BL^2/\sigma$ has to be increased by factor 7!

 $\triangleright$  For same resolution  $\sigma$ , for a single solenoid, increase field to 6 T in 12 m bore!

#### Also need low-angle coverage in forward direction

add a dipole or iron toroid for on-beam bending featuring some 10 Tm!

### **HCAL depth increase from 10 \lambda to 12 \lambda** (iron) radial thickness some 3.0 m!

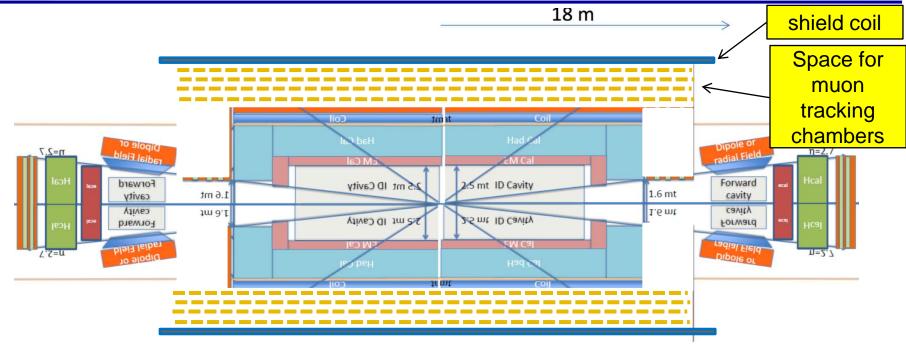
Free bore of solenoid or toroid increases to 6 m and length accordingly.

#### **ECAL to cover low angles**, move out, from 5 to 15 m, system gets longer.

Higher magnetic field, larger bore, longer system.



### **Option: Twin Solenoid + Dipoles**



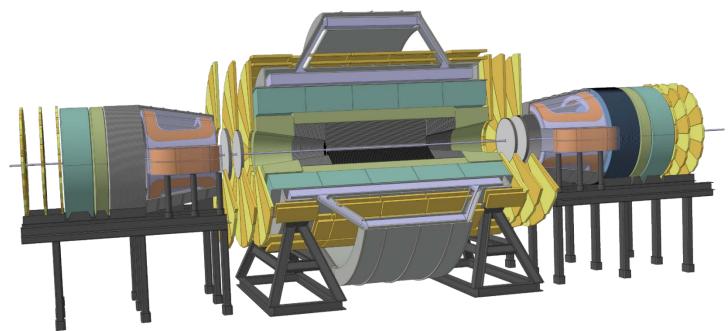
Twin Solenoid: a 6 T, 12 m dia x 23 m long main solenoid + an active shielding coil

#### **Important advantages:**

- ✓ Nice Muon tracking space: area with 2 3 T for tracking in 4-5 layers.
- ✓ Light: 2 coils + structures,  $\approx$  5 kt, only  $\approx$  4% of the option with yoke!
- ✓ Much smaller: system outer diameter is significantly less than with iron.



# **Design: 6T/12m Twin Solenoid & Dipoles**



Best performing "ultimate system" assuming same inner detector granularity of 25 micron

6T/12m actively shielded Twin Solenoid and forward dipoles

But, very expensive because of size and stored energy.

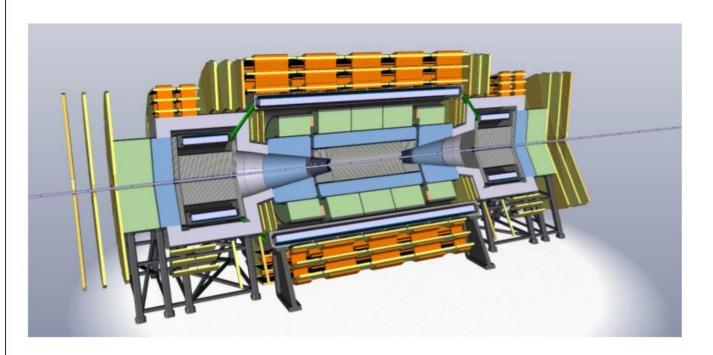
	Twin Solenoid	Dipoles
Stored energy	53 GJ	2x1.5 GJ
Total mass	7 kt	0.5 kt
Peak field	6.5 T	6.0 T
Current	80 kA	20 kA
Conductor	102 km	2 x 37 km
Bore x Length	12 m x 20 m	6 m x 6 m



### Baseline Detector 4T/10m-20m + 2 side Solenoids

### FCC-hh general purpose reference detector

100TeV pp collisions,  $L_{peak} = 3x10^{35} \text{ cm}^{-2}\text{s}^{-1}$ ,  $L_{int} = 3/30 \text{ ab}^{-1}$  25ns/5ns bunchcrossing, pileup 1000/200 per bunchcrossing

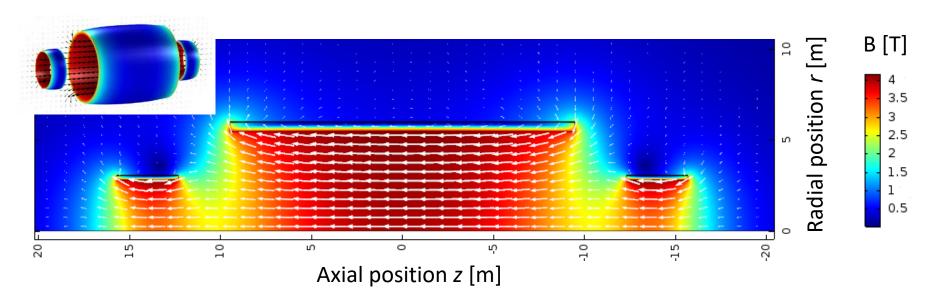


4T, 10m free bore unshielded solenoid, two 4T unshielded forward solenoids, precision spectroscopy and ECAL up to eta=4, Tracking and Calo up to eta=6

✓ Downscaling in field and bore by assuming a finer ID granularity, from 25 down to 10 micron, then 4T in 10m bore, cheaper & "affordable"



### **Unshielded Solenoid and 2 Forward Solenoids**



#### **Solenoid + Forward Solenoids**

- Forward Solenoids enhance tracking for high- $\eta$  particles
- Main solenoid: 4 T over 10 m free bore
- Forward solenoid: Free bore allowing particles at  $\eta \ge 2.5$  to pass through
- This is the approved baseline for the CDR in 2018!

Property	Value
Magnetic field in center [T]	4
Free bore diameter [m]	10
Stored energy [GJ]	13.8
Cold mass main solenoid [kt]	1.05
Cold mass forward solenoid [t]	48
Vacuum vessel mass Main Solenoid [t]	875
Vacuum vessel mass Forward Solenoid [t]	32

